Interdiffusion-Induced Polarization-Independent Optical Gain of an InGaAs–InP Quantum-Well with Carrier Effects

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Abstract—A theoretical study of the polarization-independent optical gain using group V sublattice interdiffusion in InGaAs–InP quantum wells (QW’s) is presented here. The reverse bias and carrier effects on the subband structures, transition energy, and optical gain of the interdiffused QW are discussed. The interdiffused QW structures are optimized in terms of their subband structure, carrier density, structural parameters, and properties of optical gain spectra. The results show that an optimized interdiffused QW structure can produce polarization-independent optical gain over a range of operation wavelengths around 1.5 μm, although the differential gain and linewidth enhancement factor are slightly degraded. The required tensile strain for the polarization-independent optical properties of a lattice-matched QW structure may be generated using interdiffusion. These results suggest that polarization-independent optical devices can be fabricated using interdiffusion in a lattice-matched InGaASP QW structure.

Index Terms—Carrier effects, diffused quantum well, optical gain, optical polarization independence quantum well, reverse bias effects, quantum-well amplifier.

I. INTRODUCTION

DIFFERENT types of quantum wells (QW’s) have been used as the active region of optical devices because of their enhanced optical properties, as compared to conventional bulk materials. However, quantum confinement effects break the symmetry of the electron–hole dipole and produce the TE and TM polarization dependence of the QW optical properties, including their optical gain, absorption coefficient, and refractive index when the incident light is parallel to the plane of the QW structure [1]. This is a well-known inherent feature of conventional QW’s and a disadvantage for their use in optical communication systems. For strained QW materials, such as an InGaAsP QW, polarization independence is achieved by merging the heavy hole (HH) and light hole (LH) by generating a tensile strain in the well. There are two possible ways to induce this tensile strain to produce polarization-independent optical devices, such as optical amplifiers [2], [3], optical modulators [4], [5], and waveguides [6]: one can either tailor the sublattice compositions in the well of an as-grown QW structure [2], [4] or use an interdiffused QW to produce the tensile strain in the well [3], [5]. Previously, the polarization-independent electroabsorption InGaAsP interdiffused QW modulator was proposed using a subband model without valence band mixing and carrier effects [5]. With an extended band mixing model solved self-consistently with Poisson’s equation, the details of the interdiffusion induced polarization independence in InGaAsP interdiffused QW’s, including the effects of interdiffusion and free carriers on the subband structures, optical matrix elements, and optical gain of the interdiffused QW, are reported here. However, their effects on the polarization-independent interdiffused QW structures have not been analyzed previously.

In this paper, a theoretical study of the polarization-independent gain of an InGaAs–InP QW using interdiffusion is carried out. The effects of interdiffusion on the subband structure, photon energy, and optical gain are analyzed. Taking into account free-carrier screening effects, the modification of the interdiffused QW optical properties due to different carrier densities, applied fields, and QW structure parameters (i.e., well width Lz and atomic composition) are discussed. The polarization-independent gain of the optimized interdiffused QW structures is also presented.

II. MODEL

The model of the interdiffusion is group V two-phase interdiffusion [7], [8] where only the group V elements in InGaAsP are involved and the diffusion coefficients of these elements in the barriers and wells are different so that “two-phase” interdiffusion is obtained. For a QW heterostructure, where the InGaAs well is sandwiched between two InP barriers, the interdiffusion process can be represented by a set of diffusion equations for each species. This is defined as follows:

$$\frac{\partial \xi(z,t)}{\partial t} = D_i \frac{\partial^2 \xi(z,t)}{\partial z^2}$$

(1)

where z is the growth direction, t is the annealing time, the subscript i denotes the barrier for $|z| \geq L$ or the well for $|z| < L$. L is the position of the as-grown QW interface from the well center ($z = 0$), and $\zeta$ and D are the concentration of the diffusion species and their diffusion coefficients, respectively. In solving this partial differential equation, two continuity conditions must be satisfied at the well–barrier interfaces (i.e.,
Equation (2) models the discontinuous \( k \neq 1 \) concentration at the interface while (3) expresses the flux continuity. Further details have been thoroughly discussed elsewhere [8]. Equation (1) is solved using a finite difference method to obtain the concentration distribution of the diffused species after an annealing time \( t \). This concentration ratio gives the spatial molar fraction (composition) of the interdiffused As concentration in the InGaAsP interdiffused QW structure. The parameter \( x_0 \) is the concentration of the In atoms (Group III composition) and, since the interdiffusion only involves Group V composition, \( x_0 \) is a constant. The molar fractions \( x_0 \) and \( y_0 \) are used to determine the material parameters, including the carrier effective masses and potential profiles in modeling the QW subband structures. The induced tensile strain strongly depends on the extent of the interdiffusion. The various stages of interdiffusion can be obtained by varying \( t \) and the temperature, where the temperature affects the diffusion coefficients.

The coupling of an HH and an LH is considered using the 4x4 Luttinger–Kohn Hamiltonian [9]. With effective mass theory, the Hamiltonian for the interdiffused QW valence band can be written as (4), shown at the bottom of the page, where

\[
P = \frac{\hbar^2}{2m_o} \gamma_1 \left( k_x^2 + k_y^2 - \frac{\partial}{\partial z^2} \right)
\]

\[
Q = \frac{\hbar^2}{2m_o} \gamma_2 \left( k_x^2 + k_y^2 + 2 \frac{\partial}{\partial z^2} \right)
\]

\[
V_{HH}(z) = V^V(z) - |e|Fz + |e|\varphi(z)
\]

\[
V_{LH}(z) = V^V(z) - |e|Fz + |e|\varphi(z)
\]

\[
\Omega = -\frac{\hbar^2}{m_o} \left( \frac{\sqrt{3}}{2} \gamma_3 (k_x - ik_y)^2 \right)
\]

\[
-\frac{\sqrt{3}}{4} (\gamma_3 - \gamma_2) (k_x + ik_y)^2
\]

and

\[
B = \sqrt{3} \frac{\hbar^2}{m_o} \gamma_3 (k_x - ik_y) \left( -i \frac{\partial}{\partial z} \right)
\]

where \( z \) denotes the growth direction, \( V^V(z) \) is the diffused potential profile of the valence band, and \( F \) and \( \varphi(z) \) are the applied electric field and the potential due to carriers, respectively. \( Q_c \) is the conduction band offset ratio. \( S_{1,2,3} \) and \( S_{1,2} \) are the biaxial component of strain and the splitting energy of the HH and LH induced by the uniaxial component of the strain, respectively, and the well center is defined as \( z = 0 \). Details of the relationships between \( S_{1,2} \) and \( S_{1,2} \) are given in [10]. Also, \( m_o \) is the electron mass, \( \gamma_1, \gamma_2 \), and \( \gamma_3 \) are the Luttinger–Kohn parameters [11], where \( \gamma = \frac{1}{3} (\gamma_2 + \gamma_3) \) and \( k_0^2 = k_0^2 + k_0^2 \). The fourfold degenerate block envelope functions that satisfy (4) have quantum numbers \( -3/2, -1/2, 1/2, \) and \( 3/2 \) (HH = \pm 3/2, LH = \pm 1/2). For simplicity, the axial approximation, which assumes that \( \gamma_2 = \gamma_3 \), is applied to the \( \Omega \) term [12], [13], and the 4x4 Hamiltonian is transformed into two 2x2 Hamiltonians, \( H^U \) and \( H^L \), using the framework in [13]–[15]

\[
H^\delta = \left[ \begin{array}{cc} P + Q + V_{HH}(z) & \xi \xi^* \\ \xi^* & P - Q + V_{LH}(z) \end{array} \right]
\]

where the superscript \( \delta = U \) or \( L \) and \( \xi = \Omega + i|B| \). Equation (5) is solved using a finite difference method.

The conduction band at the \( \Gamma \)-valley \( (k_0 = 0) \) is modeled using the one-dimensional, one particle Schrödinger-like equation [16] obtained from an envelope function approximation [17] through a BenDenial and Duke model [18]

\[
\frac{d^2}{dz^2} \psi_{\alpha}(z) + \frac{1}{m^*_{\alpha}} \frac{d}{dz} \frac{1}{z(z + \epsilon(z))} \psi_{\alpha}(z) = E_{\alpha} \psi_{\alpha}(z)
\]

where \( E_{\alpha}(z) \) is the diffused potential profile of the conduction band, \( m^*_{\alpha}(z) \) is the effective mass of the electron, and \( \psi_{\alpha}(z) \) represents the envelope wavefunction of an electron to the \( \alpha \)th confined subband state with an energy \( E_{\alpha} \).

The potential due to carriers \( \varphi(z) \) can be obtained by solving Poisson’s equation self-consistently with (5) and (6)

\[
\frac{d^2}{dz^2} \varphi(z) = -\frac{1}{\epsilon} \left[ p(z) - n(z) + N_D(z) - N_A(z) \right]
\]

where \( \epsilon \) is the dielectric constant of InGaAsP and \( N_D \) and \( N_A \) are the densities of ionized donors and acceptors, respectively. For simplification, \( N_D \) and \( N_A \) are assumed to be zero. The carrier densities \( p(z) \) and \( n(z) \) are given as

\[
p(z) = \frac{1}{2\pi} \int_{k_0} \sum_b \sum_i \left| \psi_{i,b}^V(z) \right|^2 \times (1 - f^V(E_{b}^V(k_0))) \, dk_0
\]
and
\[ n(z) = \frac{m_e k_B T}{\pi \hbar^2} \sum_a \left| \psi_a^C(z) \right|^2 \times \ln \left[ 1 + \exp\left( \frac{F_n - (E_a^C - E_a^C)}{k_B T} \right) \right] \]

where \( k_B \) and \( T \) are the Boltzmann constant and temperature, respectively, \( F_n \) is the quasi-Fermi level for the electron in the conduction subband, \( f^V_i(E_b^V) \) is the electron Fermi distribution function of the \( i \)th valence subband, and \( \psi_{i,k}^V \) is the \( i \)th envelope function in the valence subband where the subscript \( i \) is the quantum number of the fourfold degenerate hole states.

The optical gain is modeled using the density of state approach
\[ g(E) = \sum_{ab} \frac{2\pi \hbar}{(2\pi)^2 n_R \varepsilon_0 c_0} \int d^2 k_0 \left| \tilde{e} \cdot \tilde{P}_{ab}(k_0) \right|^2 \]
\[ \delta(E_0^C(k_0) - E_0^V(k_0) - E) \times \left[ f^C_i(E_0^C(k_0)) - f^V_i(E_0^V(k_0)) \right] \]

where \( c, n_R, \) and \( q \) are the speed of light in vacuum, refractive index, and electric charge, respectively, \( E \) is the photon energy, \( \tilde{P}_{ab} \) is the optical matrix element for a transition between the \( a \)th electron subband and the \( b \)th valence subband, \( \tilde{e} \) is a unit vector along the polarization direction of the optical electric field, and \( f^C_i(E_0^C) \) is the electron Fermi distribution function in the \( a \)th conduction subband.

The squared optical matrix element for TE mode polarization is
\[ \left| \tilde{e} \cdot \tilde{P}_{ab}(k_0) \right|^2 = \left| \langle \tilde{e} | P | s \rangle \right|^2 \left\{ \left[ \left| \langle \psi_a^C | \psi_{1/2,2}^V \rangle \right|^2 + \left| \langle \psi_a^C | \psi_{3/2,2}^V \rangle \right|^2 \right] \right\} \]
\[ \frac{1}{6} \left( \left| \langle \psi_a^C | \psi_{1/2,2}^V \rangle \right|^2 + \left| \langle \psi_a^C | \psi_{3/2,2}^V \rangle \right|^2 \right)^2 \]

For TM mode polarization,
\[ \left| \tilde{e} \cdot \tilde{P}_{ab}(k_0) \right|^2 = \frac{3}{2} \left| \langle \tilde{e} | P | s \rangle \right|^2 \left\{ \left[ \left| \langle \psi_a^C | \psi_{1/2,2}^V \rangle \right|^2 \right] \right\} \]
\[ \left| \psi_a^C \right|^2 \left| \psi_{3/2,2}^V \right|^2 \]

III. RESULTS AND DISCUSSION

All InGaAs–InP interdiffused QW structures studied here are considered to be annealed at 750 °C. The diffusion coefficient of the well and barrier materials, as well as their concentration ratios, are taken from a typical structure [8]. In modeling the optical gain of an interdiffused QW structure, the full-width at half-maximum (FWHM) of the lineshape function is assumed to be 10 meV. Due to band mixing effects, the HH and LH states discussed here are the states with dominant heavy-hole and light-hole characteristics, respectively.

A. Effects of Interdiffusion

In group V two-phase interdiffusion of InGaAs–InP interdiffused QW structures studied here are considered to be annealed at 750 °C. The diffusion coefficient of the well and barrier materials, as well as their concentration ratios, are taken from a typical structure [8]. In modeling the optical gain of an interdiffused QW structure, the full-width at half-maximum (FWHM) of the lineshape function is assumed to be 10 meV. Due to band mixing effects, the HH and LH states discussed here are the states with dominant heavy-hole and light-hole characteristics, respectively.

expression:
\[ \frac{dg}{dN}(E, n) = \lim_{\Delta N \rightarrow 0} \frac{G(E, N + \Delta N) - G(E, N)}{\Delta N} \]

where \( N \) is the carrier density. The linewidth enhancement factor \( \alpha_c \) defined as the ratio of the change of refractive index with respect to the carrier density to the change of the optical gain with respect to the carrier density, is given as
\[ \alpha_c = \frac{4\pi dh_R/dN}{\lambda dg/dN} \]

where \( \lambda \) is the photon wavelength and \( dh_R/dN \) is obtained from \( dg/dN \) using the Kramers–Kronig transformation.

The gain with a spectral broadening (\( G(E') \)) of a single interdiffused QW structure at a transition energy \( E' \) is written as
\[ G(E') = \int dE' g(E') L(E - E') \]

where \( L(E - E') \) is the Lorentzian line-broadening function. The differential gain \( dg/dN \) is calculated using the following expression:
\[ \frac{dg}{dN}(E, n) = \lim_{\Delta N \rightarrow 0} \frac{G(E, N + \Delta N) - G(E, N)}{\Delta N} \]

where \( N \) is the carrier density. The linewidth enhancement factor \( \alpha_c \), defined as the ratio of the change of refractive index with respect to the carrier density to the change of the optical gain with respect to the carrier density, is given as
\[ \alpha_c = \frac{4\pi dh_R/dN}{\lambda dg/dN} \]
of interdiffusion and carriers on the C1-HH1 transition energy and TE mode gain peak of the $\text{In}_{0.53}\text{Ga}_{0.47}\text{As–InP}$ QW with a carrier density of $5 \times 10^{12}$ cm$^{-2}$ at $k_B T = 0$. The cases with and without the carrier effects are denoted by WC and WOC, respectively. GP denotes the gain peak, and $\lambda$ is the annealing time.

<table>
<thead>
<tr>
<th>case</th>
<th>$F = 0$ kV/cm</th>
<th>$F = 100$ kV/cm</th>
</tr>
</thead>
<tbody>
<tr>
<td>$t = 0$, woc</td>
<td>(eV)</td>
<td>(eV)</td>
</tr>
<tr>
<td>$t = 0$, wc</td>
<td>0.4842</td>
<td>0.3054</td>
</tr>
<tr>
<td>$t = 0.5$, woc</td>
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<td>0.3116</td>
</tr>
<tr>
<td>$t = 0.5$, wc</td>
<td>0.4980</td>
<td>0.3192</td>
</tr>
<tr>
<td>$t = 1$, woc</td>
<td>0.4900</td>
<td>0.3283</td>
</tr>
<tr>
<td>$t = 1$, wc</td>
<td>0.5062</td>
<td>0.3284</td>
</tr>
<tr>
<td>$t = 1.4$, wc</td>
<td>0.5001</td>
<td>0.3352</td>
</tr>
</tbody>
</table>

when diffusion time ($t$) increases from 0 to 1 h for both $F = 0$ and 100 kV/cm, as shown in Table I.

The transitions between the first electron and the first HH (C1–HH1) and between the first electron and the first LH (C1–LH1) at $k_B T = 0$ are shown in Fig. 2(a) where free-carrier screening effects have been included (see the details below). For the as-grown QW ($t = 0$), the HH1 and LH1 states are clearly separated. When $t$ increases, the splitting energy reduces due to the compensation of the interdiffusion-induced shear tensile strain generated in HH1 and LH1. At $t = 1.4$ h, an average tensile strain of 0.275% is generated which makes the transitions merge. For larger $t$, the tensile strain is so large that the HH1 and LH1 transitions cross over, i.e., the transition energy of C1–HH1 becomes greater than that of C1–LH1. Consequently, the polarization-independent transition with a value of 0.841 eV can be obtained at $t = 1.4$ h.

The interdiffusion also changes the dispersion of the LH1 subbands in $k_B T$ space, as shown in Fig. 2(b), when the energy of the spin-up and spin-down carriers keep close together at $k_B T \neq 0$ for both HH1 and LH1. During interdiffusion, although the induced hydrostatic tensile strain reduces the transition energy, the modification of the interdiffused QW compositions dominate the change of the transition energy so that the resultant C1–HH1 and C1–LH1 transition energies increase. Therefore, the complete HH1 and LH1 subbands at $k_B T \neq 0$ move downwards, as shown in Fig. 2(b). This suggests that interdiffusion can be used to adjust the operating wavelength of an optical device.

B. Carrier Effects with Reverse Bias

The free-carrier screening effects on the $\text{In}_{0.53}\text{Ga}_{0.47}\text{As–InP}$ interdiffused QW structure with $L_2 = 120$ Å, $t = 0.5$ h, and a carrier density of $5 \times 10^{12}$ cm$^{-2}$ are best demonstrated by the potential profile and the fundamental wavefunction of the interdiffused QW with and without free-carrier screening effects (see Fig. 1). With carrier effects and $F = 0$, the round-shaped well bottom of the interdiffused QW is pressed down, although there is no significant change in barriers and well–barrier interfaces. This results in a slight improvement of the wavefunction confinement and the peak of the wavefunction increases slightly, as compared to the interdiffused QW without the carrier effects. For an applied field ($F$) of 100 kV/cm, the carrier effects are more intuitive, the potential profile of the well bottom becomes bumpy, and the effects of reverse bias are reduced. Therefore, the wavefunction shifts toward the center of the interdiffused QW, i.e., the confinement of the wavefunction improves considerably as compared to the interdiffused QW without free-carrier screening effects.

The C1–HH1 transition energy increases when the carrier effects are considered in all interdiffused QW’s with $t = 0$ to 1 h and $F = 0$, which is due primarily to the increase of the HH1 energy as the C1 energy generally decreases (see Table I). This suggests that the difference in the transition energy with and without carrier effects is dominated by the HH1. Similar results for the C1–HH1 transition energy are also obtained for $F = 100$ kV/cm. However, here the increase in the transition energy with and without carrier effects is >20 meV for all interdiffused QW’s with $t = 0$ to 1 h as compared to 1–2 meV in the interdiffused QW’s at $F = 0$. Nevertheless, the variation of the transition energy due to carrier effects is still dominated by the HH1 subband. As shown in Fig. 3, at $F = 100$ kV/cm, the interdiffused QW valence subbands for $t = 0.5$ h increase when the carrier
The valence subband dispersion in $k_y$ space of the In$_{0.53}$Ga$_{0.47}$As–InP interdiffused QW with $L_z = 120$ Å, a carrier density of $5 \times 10^{12}$ cm$^{-2}$, and $F = 100$ kV/cm; with the carrier effects (solid line) and without the carrier effects (dash line).

Fig. 3. The valence subband dispersion in $k_y$ space of the In$_{0.53}$Ga$_{0.47}$As–InP interdiffused QW with $L_z = 120$ Å, a carrier density of $5 \times 10^{12}$ cm$^{-2}$, and $F = 100$ kV/cm; with the carrier effects (solid line) and without the carrier effects (dash line).

Since the screening effects of free carriers reduce the effect of reverse bias, spin splitting generally reduces. Consequently, the modification of the transition energy with and without carrier effects is insensitive to the extent of the interdiffusion, as shown in Table I, and carrier effects cause a blue shift of the transition energy which is dominated by the variation of the HH subbands.

The TE optical gain spectra of the interdiffused QW with $t = 0.5$ h for various applied fields are shown in Fig. 4. At $F = 0$, the difference of the optical gain spectra with and without carrier effects is small. However, at $F = 100$ kV/cm, the optical gain of the interdiffused QW with the carrier effects increases significantly and blue shifts, as compared to the interdiffused QW without the carrier effects. For interdiffused QW’s with $t = 0$ to 1 h, with carrier effects, the gain peak at $F = 0$ is reduced slightly as compared to the absence of carrier effects (see Table I). On the contrary, at $F = 100$ kV/cm, the interdiffused QW gain peak increases substantially due to the weakening of reverse bias effects and improvement of the wavefunction confinement (see Fig. 1).

C. Polarization-Independent Gain

Group V two-phase interdiffusion can be used to modify the magnitude and spectral position of the interdiffused QW optical gain and its polarization-independent properties. It should be noted that the lower energy side of a gain spectrum is denoted as its front side to simplify the discussion.

The TE and TM gain spectra of the In$_{0.53}$Ga$_{0.47}$As–InP interdiffused QW structure with $L_z = 120$ Å blue shift when $t$ increases from $t = 0$ to 2 h (see Fig. 5). At the same time, the lower energy side of the TE and TM gain spectra merge at a suitable $t$, due to the interdiffusion-induced tensile strain. Initially, the energy of the front side of the TE gain spectrum is lower than that of the TM one for the as-grown QW structure because C1–HH1 is lower than C1–LH1. When $t$ increases, the difference of the front-side energy reduces, and at $t = 0.8$ h the TE and TM gain spectra overlap, i.e., polarization-independent gain is achieved over a wavelength range from 0.78 eV to 0.84 eV. As $t$ increases further to 2 h, the TM front-side energy is lower than that of the TE mode because the lowest transition changes from C1–HH1 to C1–LH1.

It is worth noting that the required $t$ to achieve polarization-independent gain in the $x = 0.53$ structure is $\sim 0.8$ h (see Fig. 5), which is less than that predicted for the polarization-independent transition (1.4 h) [see Fig. 2(a)]. This time difference arises since the variation of the transition energy only depends on the modification of the subbands due to interdiffusion. However, the optical gain depends on the lineshape broadening factor and the different HH and LH polarization factors in the optical matrix elements, see (11) and
(a) C1–HH1. (b) C1–LH1.

The magnitude of the TE and TM gain peaks also change when \( t \) increases (see Fig. 5). When \( t = 0 \), the TE gain peak is larger than the TM one for the as-grown QW structure. However, when \( t \) increases, the TM gain peak grows and becomes the larger one, which can be explained by the variation of optical matrix elements, as shown in Fig. 6. For the as-grown QW with \( t = 0 \), the TE optical matrix elements of C1–HH1 are at its maximum when \( k_0 \rightarrow 0 \) [see Fig. 6(a)]. However, the TM optical matrix elements of both C1–HH1 and C1–LH1 \( \rightarrow 0 \) when \( k_0 \rightarrow 0 \) so that the TE gain peak is greater than the TM gain peak at \( t = 0 \). For \( t = 0.8 \) h, the TE optical matrix elements of C1–HH1 reduce when the TM optical matrix elements of C1–LH1 increase to their maximum when \( k_0 \rightarrow 0 \) (see Fig. 6). This is because the interdiffusion-induced shear tensile strain in the well increases, which moves the LH1 subband closer to the lowest subband energy [19]. Consequently, the TM optical gain peak increases to exceed the TE one after interdiffusion. These results suggest that the optical mode of the highest gain peak can be adjusted from TE to TM using interdiffusion. In addition, the threshold current of a QW laser operated at a gain peak can be increased for TE mode operation or decreased for TM mode operation using interdiffusion.

For the interdiffused QW with \( t = 0.8 \) h, the TE optical matrix elements of C1–HH1 are smaller over the entire range of \( k_0 \) from 0 to 0.06 as compared to that of the as-grown QW \( (t = 0) \). However, the TM optical matrix elements of the interdiffused QW C1–HH1 increases in the range of \( k_0 \) as compared to that of the as-grown QW (see Fig. 6). This is because the HH1 subband has more light-hole characteristics due to the band mixing effects and the LH1 subband energy moves closer to the lowest subband energy for \( t \). The variations of the optical matrix elements contribute to weakening and strengthening the TE and TM optical gain, respectively, though the corresponding photon energy changes when \( k_0 \) increases.

When the carrier density of the \( \text{In}_{0.53}\text{Ga}_{0.47}\text{As}–\text{InP} \) interdiffused QW with \( L_z = 120 \) Å and \( t = 0.8 \) h increases from \( 5 \times 10^{12} \) cm\(^{-2} \) to \( 9 \times 10^{12} \) cm\(^{-2} \), the complete TE and TM gain spectra increase, as shown in Fig. 7, because the quasi-Fermi level increases. In addition, the TE and TM gain peaks corresponding to the high-order transitions are enhanced when the carrier density increases (see Fig. 6). The second peak of TE (TM) optical gain at \( \approx 0.96 \) eV (\( \approx 1.01 \) eV) due to the C2–HH2 (C2–LH2) transitions increases when the carrier density increases to \( 9 \times 10^{12} \) cm\(^{-2} \). Consequently, the increase of the carrier density produces a higher polarization-independent gain. Using the carrier density of \( 9 \times 10^{12} \) cm\(^{-2} \) in the \( \text{In}_{0.53}\text{Ga}_{0.47}\text{As}–\text{InP} \) interdiffused QW structure, polarization-independent gains as high as \( 1750 \) cm\(^{-1} \) can be obtained for \( t = 0.8 \) h.

Polarization-independent gain up to \( 2100 \) cm\(^{-1} \) can be obtained in the gain peak region at a specific photon energy of \( 0.83 \) eV using an \( x = 0.53 \) interdiffused QW structure after annealing for 0.2 h (see Fig. 8). This polarization-independent gain is only obtained at a single wavelength where the TE and TM mode gain spectra cross each other.

D. Effects of QW Parameters

The as-grown QW parameters that can be used to modify the gain spectra are the sublattice composition and \( L_z \). When the In content decreases from \( x = 0.53 \) to \( x = 0.51 \), the
required $t$ falls from 0.8 to $\sim 0.24$ h because part of the tensile strain required to produce polarization-independent operation has already been built-in during sample growth, i.e., 0.15% strain in an In$_{0.51}$Ga$_{0.49}$As–InP QW. Since a shorter time is needed for an $x = 0.51$ interdiffused QW, less $P$ diffuses into the well region so that the C1–HH1 and C1–LH1 transition energies decrease, which results in a red-shift of the front side of the optical gain spectra (see Fig. 7). By increasing $L_z$ from 120 to 140 Å, $t$ can be reduced further to $\sim 0.1$ h since the splitting energy of HH1 and LH1 reduces when $L_z$ increases. Since $t$ and $L_z$ decrease and increase, respectively, the operating photon energy can be further reduced and the polarization-independent gain at 0.8 eV increases to $\sim 1000$ cm$^{-1}$. It is valuable to note that, in the case of interdiffused QW with $x = 0.51$ and $L_z = 120$ Å, the required $t$ of 0.24 h for polarization-independent gain is shorter than that of 0.5 h for the polarization-independent transition. This agrees with the result of the $x = 0.53$ interdiffused QW, as discussed in Section C.

The differential gain indicated the rate of increase of optical gain with the injected carrier density is shown in Fig. 9. When $t$ increases, the differential gain decreases. For the In$_{0.53}$Ga$_{0.47}$As–InP interdiffused QW with $L_z = 120$ Å, the differential gain for the TE and TM modes are very similar for a short time between 0.2 and 0.25 h. The rate of increase of the polarization independent differential gain is about $1.3 \times 10^{-9}$ cm at $t = 0.25$ h. When $t$ increases, the TM differential gain is larger than that for the TE one but both saturate for long times, greater than 1 h. Consequently, although the differential gain decreases and the performance degrades when $t$ increases, only a short time (0.24 h) is required to produce polarization-independent gain for the $x = 0.51$ interdiffused QW [see Fig. 9(a)] so that the degradation is not significant. Similar features can also be obtained for the $x = 0.53$ interdiffused QW with $t = 0.8$ h so that the differential gain of this structure is $\sim 0.15 \times 10^{-9}$ cm, although it is not detailed here.

As shown in Fig. 9(b), the linewidth enhancement factor $\alpha$ increases when $t$ increases. However, since only a short $t$ is needed for the polarization-independent gain, $\alpha$ does not increase significantly. For the $x = 0.51$ interdiffused QW with $L_z = 120$ Å and $t = 0.24$ h, $\alpha$ is 8 but is $\sim 5$ for the as-grown one at a photon energy of 0.82 eV. For the $x = 0.51$ interdiffused QW with $L_z = 140$ Å and $t = 0.1$ h, $\alpha$ is 7.5 whereas it is $\sim 7$ for the as-grown one at a photon energy of 0.8 eV. Therefore, there is an acceptable degradation in both the differential gain and $\alpha$ for the optimized interdiffused QW structures.

E. Effects of Reverse Bias

The field-induced quantum-confined Stark shift of the optical gain of the In$_{0.53}$Ga$_{0.47}$As–InP interdiffused QW’s with $L_z = 120$ Å and $t = 0$ and 0.8 h is shown in Fig. 10. For $F = 100$ kV/cm, both the as-grown QW and the interdiffused QW can provide gain switching. The operating wavelength can be adjusted using interdiffusion, although the change of the interdiffused QW gain with applied field at the TE gain peak (250 cm$^{-1}$) is weaker than that of the as-grown QW (500 cm$^{-1}$).

Even though the polarization-independent gain can be maintained under an applied field of $F = 0$ and 100 kV/cm, polarization-independent gain and polarization-independent gain switching may not be very important for lasers because lasers are usually linearly polarized and the presence of polarization-independent gain may make the laser less stable due to mode hopping [20]. However, polarization
As InP and In$_{10}$Ga$_{90}$ due $cm$ increases, $˚A$ and Ga$_{90}$. The optimized increases, in comparison to the corresponding case 

The required time for polarization-independent gain is shorter 

Polarization-independent gain can be obtained for these in-

IV. CONCLUSION

In this paper, polarization-independent-interdiffused QW optical gain using interdiffusion has been investigated theo-

REFERENCES


[8] K. Mukai, M. Sugawara, and S. Yamazaki, “Interdiffusion process in lattice-matched In$_{0.53}$Ga$_{0.47}$As–InP and In$_{0.53}$Ga$_{0.49}$As–InP interdiffused QW structures. Taking into account free-carrier screening effects, the transition energy increases as compared to that without the carrier effects, and the blue shift is enhanced when the applied field is increased. The increasing transition energy is dominated by increasing the hole subband. With the consideration of carrier effects, the gain magnitude of an interdiffused QW slightly reduces for $F = 0$ and increases when $F$ increases, in comparison to the corresponding case without carrier effects.

Polarization-independent gain can be obtained for these interdiffused QW structures over a wavelength range of 10 meV. The required time for polarization-independent gain is shorter than that of polarization-independent transition. When the carrier density increases, the polarization-independent gain increases. The maximum polarization-independent gain is 1800 cm$^{-1}$ for a carrier density of $9 \times 10^{12}$ cm$^{-2}$. The optimized In$_{0.53}$Ga$_{0.47}$As–InP interdiffused QW with $L_z = 140$ A and $t = 0.1$ h can operate at 0.8 eV (1.55 $\mu$m) with polarization-independent gain of 1000 cm$^{-1}$, while the differential gain

and the linewidth enhancement factor of the polarization-independent interdiffused QW reduces and increases, respectively, without a significant degradation. For the as-grown lattice-matched QW structure, all the required tensile strain for the polarization independence can be generated using interdiffusion. This indicates the possibility that polarization-independent longitudinal-type optical devices can be fabricated using a lattice-matched InGaAsP QW structure and interdiffusion technology.

The highest gain peak of the QW can be varied from the TE mode to the TM mode using interdiffusion. When $t$ increases, the TE gain peak which is the largest at $t = 0$ reduces and the TM gain peak increases over the TE peak when $t \geq 0.5$ h due to the increase of the interdiffusion-induced shear tensile strain in the well. Moreover, for InGaAsP QW lasers, the threshold current can be increased for TE mode operation and reduced for TM mode operation using interdiffusion.


1986.


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